

Article

Output Tracking Control for High-Order Nonlinear Systems with Time Delay via Output Feedback Design

Keylan Alimhan ^{1,2,*} , Orken J. Mamyrbayev ^{2,*} , Gaukhar A. Abdenova ¹  and Almira Akmetkalyeva ¹

¹ Faculty of Mechanics and Mathematics, L.N. Gumilyov Eurasian National University, Nur-Sultan 010000, Kazakhstan; gauhar.phd@gmail.com (G.A.A.); almira_vko@mail.ru (A.A.)
² Institute of Information and Computational Technologies, Almaty 050010, Kazakhstan
 * Correspondence: keylan@live.jp (K.A.); morkenj@mail.ru (O.J.M.)

Abstract: Design approach of an output feedback tracking controller is proposed for a class of high-order nonlinear systems with time delay. To deal with the time delays, an appropriate Lyapunov–Krasovskii the tracking analysis is ingeniously constructed, and an output feedback tracking controller is designed by using a homogeneous domination method. It is shown that the proposed output controller independent of time delay can make the tracking error be adjusted to be sufficiently small and render all the trajectory of the closed-loop system as bounded. An example is given to illustrate the effectiveness of the proposed method.

Keywords: practical tracking; time delay; high-order nonlinear systems; output feedback; Lyapunov–Krasovskii functional



Citation: Alimhan, K.; Mamyrbayev, O.J.; Abdenova, G.A.; Akmetkalyeva, A. Output Tracking Control for High-Order Nonlinear Systems with Time Delay via Output Feedback Design. *Symmetry* **2021**, *13*, 675.
<https://doi.org/10.3390/sym13040675>

Academic Editor: Jan Awrejcewicz

Received: 2 March 2021
 Accepted: 8 April 2021
 Published: 13 April 2021

Publisher’s Note: MDPI stays neutral with regard to jurisdictional claims in published maps and institutional affiliations.



Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (<https://creativecommons.org/licenses/by/4.0/>).

1. Introduction

In the field of nonlinear control, stabilization and output tracking problems are two of the most important and challenging problems. In this paper, we mainly focus on an output feedback practical tracking problem for a class of high-order time delay nonlinear systems of the form:

$$\begin{aligned} \dot{x}_i(t) &= x_{i+1}(t)^{p_i} + \varphi_i(t, x(t), x(t-d), u(t)), \quad i = 1, \dots, n-1, \\ \dot{x}_n(t) &= u + \varphi_n(t, x(t), x(t-d), u(t)), \\ y(t) &= x_1(t) - y_r(t) \end{aligned} \tag{1}$$

where $x(t) = (x_1(t), \dots, x_n(t))^T \in R^n$, $u(t) \in R$, and $y(t) \in R$ are states, input, and output of the system. Corresponding to this, $y_r(t) \in R$ is a given unmeasurable reference signal. The constant $d \geq 0$ is a given time delay parameter of the system, and the system initial condition is $x(\theta) = \varphi_0(\theta)$, $\theta \in [0, d]$. The nonlinear function $\varphi_i(\cdot)$ is a continuous function, and $p_i \in R_{odd}^{\geq 1} := \{p/q \in [0, \infty) : p \text{ and } q \text{ are odd integers, } p \geq q, (i = 1, \dots, n-1)\}$.

The practical output tracking problem of a nonlinear system (1) has received a great deal of attention over the past years, and many important results have been achieved. The work [1] by Celikovsky and Huang studied the local output tracking problem. Because it is not suitable for a global case, in [2], the problem of global output tracking was considered. The work [3] investigated the adaptive practical output tracking problem. Later, in [4–14], the above works are extended to more general cases under some weak conditions.

It has been known that solving the above problem via output feedback design for high-order nonlinear systems is very challenging and difficult compared to the state feedback case. Because there is no general and effective method to design a non-linear observer, the theory of output feedback control design developed more slowly. Recently, some results were reported, for example, [6–11].

However, most of the above results do not consider the effect of time delay. It is well known that time delay phenomenon is ubiquitous and inevitable in nature, which is

one of the main reasons for the instability of system performance. Therefore, the design of a controller for stabilization and output tracking problems of nonlinear systems with time delay has important significance in the field of control engineering. Thus, there is little coverage on this issue. In [15–18], we only solved the problem by state feedback control. Lyapunov–Krasovskii method is a powerful tool in stability analysis and controller design for time delay systems in [19–26]. Study for the output tracking control time delay problem developed more slowly than the stabilization case with time delay. For the output tracking time delay problems via output feedback, there are some new interesting works (see [27–30]). However, these results only investigate the case p_i equal one for considered systems (1). For a high-order time delay nonlinear system (1), the output tracking problem becomes more complicated and difficult to solve. However, to the best of our knowledge, the global practical output problem of nonlinear systems with partial unmeasured states and time delay via output feedback have not yet been considered to date, which motivates this research.

This paper mainly studies the output tracking control problem for a class of high-order nonlinear systems with time delay by using the output feedback domination approach.

The main contributions of this work can be summarized as follows: (i) it should be noticed that the output feedback tracking control problem for high-order nonlinear systems has been mainly studied in [2–11]. However, by the introduction of time delay factors, the output feedback tracking control problem for the high-order nonlinear system is first studied in this paper by using a homogeneous domination method [31–33]; (ii) by comparison with the case $p_i = 1$ in [27–30], how to construct an appropriate Lyapunov–Krasovskii functional for high-order nonlinear system (1) is a non-trivial work. A new Lyapunov–Krasovskii functional for solving the practical output tracking problem is constructed.

Works [34,35] investigated a finite-time output feedback stabilization problem for stochastic high-order nonlinear systems, and work [36] studied a global finite-time control problem for a class of switched nonlinear systems with different powers via output feedback. However, these results do not consider effect of time delay.

This paper addresses the output feedback tracking problem of a class of high-order nonlinear time delay systems. However, if a general nonlinear system or a nonlinear symmetric system can be transformed into the considered system in this article, then the method proposed in this article can also be used.

Throughout the paper, we adopt such notations: R denotes the set of all real numbers, R^+ denotes the set of positive real numbers, and R^i represents the i -dimensional Euclidean space. $\|x\|$ denotes the Euclidean norm of vector $x(t)$. For any vector $x(t) \in R^n$, denote $\bar{x}_i(t) := (x_1(t), \dots, x_i(t))^T \in R^i, i = 1, \dots, n$.

2. Mathematical Preliminaries

Several lemmas are used throughout this paper. We first give the definition of homogeneous function related to the following two lemmas.

Definition 1 ([31]). For a set of coordinates $x = (x_1, \dots, x_n) \in R^n$ and a n -tuple of positive real numbers $r = (r_1, \dots, r_n)$.

- (i) The dilation $\Delta_s^r(x)$ is defined by $\Delta_s^r(x) = (s^{r_1}x_1, \dots, s^{r_n}x_n), \forall s > 0$, with r_i being called as the weights of the coordinate. For simplicity, we define dilation weight $\Delta = (r_1, \dots, r_n)$.
- (ii) A function $V : R^n \rightarrow R$ is said to be homogeneous of degree m ($m \in R$) if $V(\Delta_s^m(x)) = s^m V(x_1, \dots, x_n), \forall s > 0, \forall x \in R^n / \{0\}$.
- (iii) A vector field $f = (f_1, \dots, f_n)^T : R^n \rightarrow R^n$ is said to be homogeneous of degree k if the component f_i is homogeneous of degree $k + r_i$ for each i , that is, $f_i(s^{r_1}x_1, \dots, s^{r_n}x_n) = s^{k+r_i}f_i(x_1, \dots, x_n), \forall s > 0, \forall x \in R^n / \{0\}, i = 1, \dots, n$.
- (iv) $\|x\|_{\Delta,p} = (\sum_{i=1}^n |x_i|^{p/r_i})^{1/p}, \forall x \in R^n, p \geq 1$ denote a homogeneous p -norm. For simplicity, write $\|x\|_{\Delta}$ for $\|x\|_{\Delta,2}$.

Lemma 1 ([31]). Denote Δ as dilation weight, and suppose $V_1(x)$ and $V_2(x)$ are homogeneous functions with degree m_1 and m_2 , respectively. Then, $V_1(x)V_2(x)$ is still a homogeneous function with degree of $m_1 + m_2$ with respect to the same dilation weight.

Lemma 2 ([31]). Suppose $V : R^n \rightarrow R$ is a homogeneous function of degree m with respect to the dilation weight Δ . Then, the following statements hold:

- (i) $\partial V / \partial x_i$ is homogeneous of degree $m - r_i$ with r_i being the homogeneous weight of x_i .
- (ii) There is a constant $\bar{\sigma} > 0$ such that $V(x) \leq \bar{\sigma} \|x\|_{\Delta}^m$. Moreover, if $V(x)$ is positive definite, there is a constant $\underline{\sigma} > 0$ such that $\underline{\sigma} \|x\|_{\Delta}^m \leq V(x)$.

Lemma 3 ([33]). Let $x, y \in R$ and $p \geq 1$ be an integer. Then:

$$|x + y|^p \leq 2^{p-1}|x^p + y^p|, (|x| + |y|)^{1/p} \leq |x|^{1/p} + |y|^{1/p} \leq 2^{(p-1)/p}(|x| + |y|)^{1/p}$$

If p is an odd positive integer, then,

$$|x - y|^p \leq 2^{p-1}|x^p - y^p|, |x^{1/p} - y^{1/p}| \leq 2^{(p-1)/p}|x - y|^{1/p}.$$

Lemma 4 ([33]). For any positive real numbers, c, d , and any real-valued function $\gamma(x, y) > 0$, the following holds

$$|x|^c |y|^d \leq \frac{c}{c+d} \gamma(x, y) |x|^{c+d} + \frac{d}{c+d} \gamma^{-c/d}(x, y) |y|^{c+d}$$

3. Problem Formulation and Key Assumptions

In this paper, our objective is to provide a solution to global practical output tracking of a system (1) via using the output feedback controller of the following form

$$\begin{aligned} \dot{\zeta} &= \alpha(\zeta, y), \zeta \in R^m \\ u(t) &= g(\zeta, y), \end{aligned} \quad (2)$$

such that, for any $\varepsilon > 0$ and every $x(0) \in R^n$, there exists a finite time $T(\varepsilon, x(0)) > 0$ rendering the tracking error of the closed-loop system (1) and (2), thus it satisfies

$$|y(t)| = |x_1(t) - y_r(t)| < \varepsilon, \forall t \geq T > 0 \quad (3)$$

and all states of the closed-loop system (1) and (2) are well defined and globally bounded on $[0, \infty)$.

To make this possible, the following assumptions are imposed on system (1) and reference signal $y_r(t)$.

Assumption 1. There exist positive constants C_1, C_2 , and $\tau \geq 0$ such that:

$$\begin{aligned} |\varphi_i(t, x(t), x(t-d), u(t))| &\leq C_1 \left(|x_1(t)|^{(r_i+\tau)/r_1} + |x_2(t)|^{(r_i+\tau)/r_2} + \dots + |x_i(t)|^{(r_i+\tau)/r_i} \right. \\ &\quad \left. + |x_1(t-d)|^{(r_i+\tau)/r_1} + |x_2(t-d)|^{(r_i+\tau)/r_2} + \dots + |x_i(t-d)|^{(r_i+\tau)/r_i} \right) + C_2 \end{aligned} \quad (4)$$

where r_i ($i = 1, \dots, n$) are defined so as to satisfy:

$$r_1 = 1, r_i p_{i-1} = \tau + r_{i-1} \quad (5)$$

Remark 1. Unlike the conditions in [6–9], Assumption 1 contains time delay terms. Further, when p_i equals one, the assumption becomes an important hypothesis in literature [27].

Assumption 2. For the reference function $y_r(t)$ and its derivative, there exists a constant $D > 0$ such that:

$$\max\{|y_r(t)|, |\dot{y}_r(t)|\} \leq D, \forall t > 0$$

Remark 2. Assumption 2 indicates condition for the reference signal $y_r(t)$. It is a standard condition for solving the practical output tracking problem of nonlinear systems in [2–13,23,25,26].

Next, we construct an output feedback controller for system (1) under Assumptions 1 and 2. To achieve this goal, we first construct an output feedback controller for the nominal system of system (1) by setting $\phi_i(t, x, u) = 0$, $i = 1, \dots, n$, i.e., the following nominal system:

$$\dot{z}_i(t) = z_{i+1}^{p_i}(t), \quad i = 1, \dots, n-1, \quad \dot{z}_n(t) = v(t), \quad y(t) = z_1(t) \quad (6)$$

where $p_i \in \mathbb{R}_{\text{odd}}^{\geq 1}$ for $i = 1, \dots, n-1$.

Our control objective is to find a controller of the form:

$$\begin{aligned} \dot{\eta} &= \alpha(\eta, y), \quad \eta \in \mathbb{R}^{n-1} \\ v(t) &= g(\eta, y), \end{aligned} \quad (7)$$

with continuous functions $\alpha: \mathbb{R}^n \rightarrow \mathbb{R}^{n-1}$ and $v: \mathbb{R}^n \rightarrow \mathbb{R}$ satisfying $\alpha(0, 0) = 0$, $g(0, 0) = 0$ such that the closed-loop system (6) and (7) is globally asymptotically stable.

Using a similar approach as in [7,32], we construct an output feedback controller for system (6), which can be described in the following proposition.

Proposition 1 ([7,32]). For the system (6), suppose there exists an output controller based on observer.

$$v(\hat{z}) = -\beta_n[\hat{z}_n^{\mu/r_n} + \beta_{n-1}\{\hat{z}_{n-1}^{\mu/r_{n-1}} + \dots + \beta_2(\hat{z}_2^{\mu/r_2} + \beta_1 z_1^{\mu/r_1}) \dots\}]^{(r_n+\tau)/\mu} \quad (8)$$

$$\begin{aligned} \dot{\eta}_2 &= -L_1 \hat{z}_2^{p_1}, & \hat{z}_2 &= [\eta_2 + L_1 z_1]^{r_2/r_1} \\ \dot{\eta}_k &= -L_{k-1} \hat{z}_k^{p_{k-1}}, & \hat{z}_k &= [\eta_k + L_{k-1} \hat{z}_{k-1}]^{r_k/r_{k-1}}, \quad k = 3, \dots, n \end{aligned} \quad (9)$$

with a positive definite, C^1 , and radially unbounded Lyapunov function,

$$\begin{aligned} V &= V_1 + V_2, \\ V_1 &= \sum_{i=1}^n \int_{z_i^*}^{z_i} (s^{\mu/r_i} - z_i^{*\mu/r_i})^{(2\mu-\tau-r_i)/\mu} ds, \\ V_2 &= \sum_{i=1}^n \int_{(\eta_i+L_{i-1}z_{i-1})}^{z_i} (s^{r_{i-1}/(2\mu-\tau-r_{i-1})} - (\eta_i + L_{i-1}z_{i-1}))^{(2\mu-\tau-r_{i-1})/r_{i-1}} ds \end{aligned} \quad (10)$$

such that:

$$\dot{V} \leq -\frac{1}{4} \sum_{j=1}^n \zeta_j^2 - \frac{1}{4} \sum_{j=2}^n \zeta_j^2 \quad (11)$$

where $\hat{z} = [\hat{z}_1, \hat{z}_2, \dots, \hat{z}_n]^T \in \mathbb{R}^n$, $\hat{z}_1 = z_1 = y$ and r_i ($i = 2, \dots, n+1$) are defined by (5) and $L_i > 0$ ($i = 1, \dots, n-1$) are the gains to be selected later, and:

$$\zeta_i = z_i^{\mu/r_i} - z_i^{*\mu/r_i}, \quad z_i^* = -\beta_{i-1}^{r_i/\mu} \zeta_{i-1}^{r_i/\mu}, \quad z_1^* = 0, \quad \zeta_i = (z_i^{p_{i-1}} - \hat{z}_i^{p_{i-1}})^{\mu/p_{i-1}},$$

$\mu \geq \max_{1 \leq i \leq n} \{\tau + r_i\}$ and $\beta_i > 0$, $i = 1, \dots, n$ are constants. Then, the closed-loop system (6), (8), and (9) is globally asymptotically stable.

Since the proof of the proposition is exactly the same [11,33], it is omitted here.

Note that, from (10), it is easy to verify that $V > 0$ and is radially unbounded with respect to:

$$Z := [z_1, \dots, z_n, \eta_2, \dots, \eta_n]^T \quad (12)$$

Denoting the dilation weight:

$$\Delta = \underbrace{[r_1, r_2, \dots, r_n]}_{\text{for } z_1, \dots, z_n} \underbrace{[r_1, r_2, \dots, r_{n-1}]}_{\text{for } \eta_2, \dots, \eta_n} \tag{13}$$

the closed-loop system (6) with the output controller (8) and (9) can be rewritten in a compact form as:

$$\dot{Z} = F(Z) = [z_2^{p_1}, \dots, z_n^{p_{n-1}}, v(z_1, \eta_2, \dots, \eta_n), f_{n+1}, \dots, f_{2n-1}]^T \tag{14}$$

where $f_{n+1} := \dot{\eta}_2, f_{n+2} := \dot{\eta}_3, \dots, f_{2n-1} := \dot{\eta}_n$.

By Definition 1, we can prove that $F(Z)$ is homogeneous of degree τ and $V(Z)$ is homogeneous of degree $2\mu - \tau$ with respect to dilation weight Δ . By Lemma 4, the following holds:

$$\frac{\partial V(Z)}{\partial Z_i} \leq \gamma_1 \|Z\|_{\Delta}^{2\mu - \tau - r_i}, \quad \gamma_1 > 0, \text{ for } i = 1, \dots, n \tag{15}$$

In addition, by Proposition 1, closed-loop system (8), (14) and (9) is globally asymptotically stable. Therefore, the following holds:

$$\dot{V}(Z) \Big|_{(14)} = \frac{\partial V(Z)}{\partial Z} F(Z) \leq -\gamma_2 \|Z\|_{\Delta}^{2\mu} \tag{16}$$

where $\gamma_2 > 0$ is a constant and $\|Z\|_{\Delta} = \sqrt{\sum_{i=1}^{2n-1} |Z_i|^{2/r_i}}$.

4. Output Tracking Control via Output Feedback Design

In this section, we state and prove our result.

Theorem 1. Consider system (1) under Assumptions 1 and 2. For any given delay constant d , the global practical output tracking problem stated above is solvable by an output feedback of the form (7), and a design method for such a control is explicitly given.

Proof. First, we define a change of coordinates:

$$z_1(t) := y(t), \quad M^{\kappa_i} z_i(t) := x_i(t), \quad i = 2, \dots, n, \quad M^{\kappa_n+1} v(t) := u(t) \tag{17}$$

where $\kappa_1 = 0, \kappa_i = (\kappa_{i-1} + 1) / p_{i-1}, i = 2, \dots, n$ and constant gain $M \geq 1$ are determined later. Under (17), system (1) can be rewritten in variables z_i as:

$$\begin{aligned} \dot{z}_i(t) &= M z_{i+1}^{p_i}(t) + \psi_i(t, z(t), z(t-d), v(t)), \quad i = 1, \dots, n-1, \\ \dot{z}_n(t) &= M v(t) + \psi_n(t, z(t), z(t-d), v(t)), \\ y(t) &= z_1(t) \end{aligned} \tag{18}$$

where:

$$\begin{aligned} \psi_1(t, z(t), z(t-d), v(t)) &:= \varphi_1(t, x(t), x(t-d), u(t)) - \dot{y}_r(t) \\ \psi_i(t, z(t), z(t-d), v(t)) &:= \frac{\varphi_i(t, x(t), x(t-d), u(t))}{M^{\kappa_i}}, \quad i = 2, \dots, n. \end{aligned} \tag{19}$$

By Assumption 1, Lemma 3, and $M \geq 1$, it is not difficult to get the following to hold:

$$\begin{aligned} |\psi_1(z_1(t), z_1(t-d))| &\leq C_1 \left(|z_1(t) + y_r(t)|^{(r_1+\tau)/r_1} + |z_1(t-d) + y_r(t-d)|^{(r_1+\tau)/r_1} \right) + C_2 + |\dot{y}_r| \\ |\psi_i(\bar{z}_i(t), z_1(t-d), \dots, z_i(t-d))| &= \left| \frac{\varphi_i(\bar{x}_i(t), x_1(t-d), \dots, x_i(t-d))}{M^{\kappa_i}} \right| \\ &\leq \frac{C_1}{M^{\kappa_i}} \left(|z_1(t) + y_r(t)|^{(r_i+\tau)/r_1} + |M^{\kappa_2} z_2(t)|^{(r_i+\tau)/r_2} + \dots + |M^{\kappa_i} z_i(t)|^{(r_i+\tau)/r_i} \right) \\ &\quad + \left[|z_1(t-d) + y_r(t-d)|^{(r_i+\tau)/r_1} + |M^{\kappa_2} z_2(t-d)|^{(r_i+\tau)/r_2} + \dots + |M^{\kappa_i} z_i(t-d)|^{(r_i+\tau)/r_i} \right] + \frac{C_2}{M^{\kappa_i}} \end{aligned}$$

Further, by Assumption 2, we can easily calculate:

$$\begin{aligned}
 |\psi_1(z_1(t), z_1(t-d))| &\leq \bar{C}_1 \left(|z_1(t)|^{(r_1+\tau)/r_1} + |z_1(t-d)|^{(r_1+\tau)/r_1} \right) + \bar{C}_2 \\
 |\psi_i(\bar{z}_i(t), z_1(t-d), \dots, z_i(t-d))| &\leq \bar{C}_1 M^{1-v_i} \sum_{j=1}^i \left(|z_j(t)|^{(r_i+\tau)/r_j} + |z_j(t-d)|^{(r_i+\tau)/r_j} \right) + \frac{\bar{C}_2}{M^{\kappa_i}}, \quad i = 2, \dots, n
 \end{aligned}
 \tag{20}$$

where $\bar{C}_1 > 0$, $\bar{C}_2 > 0$ only dependent on constants C_1 , C_2 , τ , κ_i and M and $v_i = \min\{1 - \kappa_j(r_i + \tau)/r_j + \kappa_i, 2 \leq j \leq i, 1 \leq i \leq n\} > 0$ are some constants.

By the definition of $r_j = \tau\kappa_j + 1/(p_1 \dots p_{j-1})$,

$$\kappa_j \frac{r_{i+1}p_i}{r_j} - \kappa_i = \frac{\tau\kappa_j + \kappa_j/p_1 \dots p_{i-1} - \kappa_i/p_1 \dots p_{j-1}}{\tau\kappa_j + 1/p_1 \dots p_{j-1}} \leq \frac{\tau\kappa_j}{\tau\kappa_j + 1/p_1 \dots p_{j-1}} < 1, \tag{21}$$

$j = 2, \dots, i, \quad i = 1, \dots, n.$

Notice that the two systems (1) and (18) are equivalent to each other, and hence, we can work on system (18) instead of system (1) whenever it is more convenient. Now, by Proposition 1, we can construct an output controller for system (18) in the form:

$$v(\hat{z}) = -\beta_n [\hat{z}_n^{\mu/r_n} + \beta_{n-1} \{ \hat{z}_{n-1}^{\mu/r_{n-1}} + \dots + \beta_2 (\hat{z}_2^{\mu/r_2} + \beta_1 z_1^{\mu/r_1}) \dots \}]^{(r_n+\tau)/\mu} \tag{22}$$

$$\begin{aligned}
 \dot{\eta}_2 &= -ML_1 \hat{z}_2^{p_1}, & \hat{z}_2 &= (\eta_2 + L_1 z_1)^{r_2/r_1} \\
 \dot{\eta}_k &= -ML_{k-1} \hat{z}_k^{p_{k-1}}, & \hat{z}_k &= (\eta_k + L_{k-1} \hat{z}_{k-1})^{r_k/r_{k-1}}, \quad k = 3, \dots, n
 \end{aligned}
 \tag{23}$$

Using (12) and (14), the closed-loop system (18), (22), and (23) can be written in the following form:

$$\dot{Z} = MF(Z) + [\psi_1(\cdot), \psi_2(\cdot), \psi_3(\cdot), \dots, \psi_n(\cdot), 0, \dots, 0]^T \tag{24}$$

Hence, adopting the same Lyapunov function (10), i.e., $V(Z)$, the time derivative of $V(Z)$ along the trajectory of (24) satisfies:

$$\begin{aligned}
 \dot{V}(Z) &= M \frac{\partial V(Z)}{\partial Z} F(Z) \\
 &\quad + \frac{\partial V(Z)}{\partial Z} [\psi_1(\cdot), \psi_2(\cdot), \psi_3(\cdot), \dots, \psi_n(\cdot), 0, \dots, 0]^T \\
 &\leq -M\gamma \|Z\|_{\Delta}^{2\mu} + \sum_{i=1}^n \frac{\partial V(Z)}{\partial Z_i} \psi_i(\cdot).
 \end{aligned}
 \tag{25}$$

Further, using (20), one obtains:

$$\begin{aligned}
 \dot{V}(Z) &\leq -M\gamma \|Z\|_{\Delta}^{2\mu} \\
 &\quad + \bar{C}_1 \sum_{i=1}^n M^{1-v_i} \left| \frac{\partial V(Z)}{\partial Z_i} \right| \left[\left(|z_1(t)|^{(r_i+\tau)/r_1} + |z_2(t)|^{(r_i+\tau)/r_2} + \dots + |z_i(t)|^{(r_i+\tau)/r_i} \right) \right. \\
 &\quad \left. + \left(|z_1(t-d)|^{(r_i+\tau)/r_1} + |z_2(t-d)|^{(r_i+\tau)/r_2} + \dots + |z_i(t-d)|^{(r_i+\tau)/r_i} \right) \right] + \bar{C}_2 \sum_{i=1}^n \frac{1}{M^{\kappa_i}} \left| \frac{\partial V(Z)}{\partial Z_i} \right|.
 \end{aligned}
 \tag{26}$$

Since, by Lemma 2 and (15), $\frac{\partial V(Z)}{\partial Z_i}$ is homogeneous of degree $2\mu - \tau - r_i$, the terms:

$$\left| \frac{\partial V(Z)}{\partial Z_i} \right| \left(|z_1|^{(r_i+\tau)/r_1} + |z_2|^{(r_i+\tau)/r_2} + \dots + |z_i|^{(r_i+\tau)/r_i} \right)$$

and:

$$\left| \frac{\partial V(Z)}{\partial Z_i} \right| \left(|z_1(t-d)|^{(r_i+\tau)/r_1} + |z_2(t-d)|^{(r_i+\tau)/r_2} + \dots + |z_i(t-d)|^{(r_i+\tau)/r_i} \right)$$

are homogeneous of degree 2μ , and, hence, it follows from Lemmas 1 and 2 that, for each $i = 1, \dots, n$, there exists constants $\widehat{\lambda}_i, \widetilde{\lambda}_i > 0$ such that:

$$\begin{aligned} & \left| \frac{\partial V(Z)}{\partial Z_i} \right| \left[\left(|z_1|^{(r_i+\tau)/r_1} + |z_2|^{(r_i+\tau)/r_2} + \dots + |z_i|^{(r_i+\tau)/r_i} \right) \right. \\ & \quad \left. + \left(|z_1(t-d)|^{(r_i+\tau)/r_1} + |z_2(t-d)|^{(r_i+\tau)/r_2} + \dots + |z_i(t-d)|^{(r_i+\tau)/r_i} \right) \right] \\ & \leq \widehat{\lambda}_i \|Z(t)\|_{\Delta}^{2\mu} + \widetilde{\lambda}_i \|Z(t-d)\|_{\Delta}^{2\mu} \end{aligned}$$

Furthermore, it follows from Lemmas 2 and 4 that there are positive constants $a_1, \bar{a}_2, \widetilde{a}_2$ such that:

$$\begin{aligned} \bar{C}_2 \left| \frac{\partial V(Z)}{\partial Z_1} \right| & \leq a_1 \|Z\|_{\Delta}^{2\mu-\tau-r_1} \\ & = a_1 \left(M^{1/2\mu} \|Z\|_{\Delta} \right)^{2\mu-\tau-r_1} \left(M^{-(2\mu-\tau-r_1)/(2\mu(\tau+r_1))} \right)^{\tau+r_1} \\ & \leq \frac{\gamma}{2} M \|Z\|_{\Delta}^{2\mu} + \bar{a}_2 M^{-(2\mu-\tau-r_1)/(\tau+r_1)}, \\ \bar{C}_2 \left| \frac{\partial V(Z)}{\partial Z_i} \right| & \leq a_1 M^{\kappa_i} \|Z\|_{\Delta}^{2\mu-\tau-r_i} \left(M^{-\kappa_i/(\tau+r_i)} \right)^{\tau+r_i} \\ & \leq M^{\kappa_i} \|Z\|_{\Delta}^{2\mu} + \widetilde{a}_2 M^{-2\mu\kappa_i/(\tau+r_i)}, \quad i = 2, \dots, n \end{aligned} \quad (27)$$

Now, substituting (27) and the above into (26) leads to:

$$\begin{aligned} \dot{V}(Z) & \leq -M\gamma \|Z\|_{\Delta}^{2\mu} \\ & \quad + \bar{C}_1 \sum_{i=1}^n M^{1-\nu_i} \left(\widehat{\lambda}_i \|Z(t)\|_{\Delta}^{2\mu} + \widetilde{\lambda}_i \|Z(t-d)\|_{\Delta}^{2\mu} \right) + \frac{\gamma}{2} M \|Z\|_{\Delta}^{2\mu} + \bar{a}_2 M^{-(2\mu-\tau-r_1)/(\tau+r_1)}, \\ & \quad + \sum_{i=2}^n \frac{1}{M^{\kappa_i}} \left(M^{\kappa_i} \|Z\|_{\Delta}^{2\mu} + \widetilde{a}_2 M^{-2\mu\kappa_i/(\tau+r_i)} \right) \\ \dot{V}(Z(t)) & \leq -M\gamma \|Z(t)\|_{\Delta}^{2\mu} \\ & \quad + \bar{C}_1 \sum_{i=1}^n M^{1-\nu_i} \left(\widehat{\lambda}_i \|Z(t)\|_{\Delta}^{2\mu} + \widetilde{\lambda}_i \|Z(t-d)\|_{\Delta}^{2\mu} \right) + \frac{\gamma}{2} M \|Z(t)\|_{\Delta}^{2\mu} + \bar{a}_2 M^{-(2\mu-\tau-r_1)/(\tau+r_1)} \\ & \quad + \sum_{i=2}^n \left(\|Z(t)\|_{\Delta}^{2\mu} + \widetilde{a}_2 M^{-2\mu\kappa_i/(\tau+r_i)-\kappa_i} \right) \\ & = -M \left[\left(\frac{\gamma}{2} - (n-1)M^{-1} - \bar{C}_1 \sum_{i=1}^n M^{-\nu_i} \widehat{\lambda}_i \right) \|Z(t)\|_{\Delta}^{2\mu} - \left(\bar{C}_1 \sum_{i=1}^n M^{-\nu_i} \widetilde{\lambda}_i \right) \|Z(t-d)\|_{\Delta}^{2\mu} \right] \\ & \quad + \bar{a}_2 M^{-(2\mu-\tau-r_1)/(\tau+r_1)} + \sum_{i=2}^n \widetilde{a}_2 M^{-(2\mu+\tau+r_i)\kappa_i/(\tau+r_i)} \\ & = -M \left[\left(\frac{\gamma}{2} - G_1(M) \right) \|Z(t)\|_{\Delta}^{2\mu} - \left(\bar{C}_1 \sum_{i=1}^n M^{-\nu_i} \widetilde{\lambda}_i \right) \|Z(t-d)\|_{\Delta}^{2\mu} \right] + a_2 G_2(M) \end{aligned} \quad (28)$$

where:

$$\begin{aligned} G_1(M) & = (n-1)M^{-1} + \bar{C}_1 \sum_{i=1}^n M^{-\nu_i} \widehat{\lambda}_i \\ G_2(M) & = a_2 \left(M^{-(2\mu-\tau-r_1)/(\tau+r_1)} + \sum_{i=2}^n M^{-(2\mu+\tau+r_i)\kappa_i/(\tau+r_i)} \right), \quad a_2 = \max(\bar{a}_2, \widetilde{a}_2) \end{aligned} \quad (29)$$

both of which are positive and monotonically decreasing to zero as M increases indefinitely.

To deal with the time delays, we construct a Lyapunov–Krasovskii functional based on Lyapunov function (10):

$$U(Z(t)) = V(Z(t)) + W(Z(t)), \quad W(Z(t)) = \left(\bar{C}_1 \sum_{i=1}^n M^{1-\nu_i} \widetilde{\lambda}_i \right) \int_{t-d}^t \|Z(s)\|_{\Delta}^{2\mu} ds \quad (30)$$

By (28) and (30), it yields:

$$\dot{U}(Z) \leq -M\frac{\gamma}{2}\|Z\|_{\Delta}^{2\mu} + M\left(G_1(M) + \bar{C}_1\sum_{i=1}^n M^{-\nu_i}\tilde{\lambda}_i\right)\|Z\|_{\Delta}^{2\mu} + a_2G_2(M) \quad (31)$$

Now, let us define:

$$\Omega = \left\{M \geq 1 \mid \frac{\gamma}{4} - G_1(M) - \bar{C}_1\sum_{i=1}^n M^{-\nu_i}\tilde{\lambda}_i > 0\right\} \quad (32)$$

and take an arbitrary $M \in \Omega$. Then, the inequality (31) becomes:

$$\dot{U}(Z) \leq -\frac{M\gamma}{4}\|Z\|_{\Delta}^{2\mu} + a_2G_2(M) \quad (33)$$

In (30), $V(Z)$ and $W(Z)$ are homogeneous of degree $2\mu - \tau$ and 2μ with respect to Δ , respectively. Hence, by Lemma 2, the following holds:

$$\lambda_1\|Z(t)\|_{\Delta}^{2\mu-\tau} \leq V(Z(t)) \leq \lambda_2\|Z(t)\|_{\Delta}^{2\mu-\tau} \quad (34)$$

and:

$$\omega_1\|Z(t)\|_{\Delta}^{2\mu} \leq W(Z(t)) \leq \omega_2\|Z(t)\|_{\Delta}^{2\mu} \quad (35)$$

where $\lambda_i > 0$, $\omega_i > 0$, $i = 1, 2$ are constants.

Moreover, by Lemma 4, we have:

$$\lambda_2\frac{M}{M}\|Z(t)\|_{\Delta}^{2\mu-\tau} = M\left(\left(\frac{\lambda_2}{M}\right)^{1/\tau}\right)^{\tau}\|Z(t)\|_{\Delta}^{2\mu-\tau} \leq \frac{2\mu-\tau}{2\mu}M\|Z(t)\|_{\Delta}^{2\mu} + \frac{\tau M^{(\tau-2\mu)/\tau}}{2\mu}\lambda_2^{2\mu/\tau} \quad (36)$$

Then, we have:

$$\omega_1\|Z(t)\|_{\Delta}^{2\mu} \leq U(Z(t)) \leq \rho_2M\|Z(t)\|_{\Delta}^{2\mu} + \frac{\tau}{2\mu M^{(2\mu-\tau)/\tau}}\lambda_2^{2\mu/\tau}, \quad (37)$$

or:

$$\frac{\omega_1\gamma}{4\rho_2}\|Z(t)\|_{\Delta}^{2\mu} \leq \frac{\gamma}{4\rho_2}U(Z(t)) \leq M\frac{\gamma}{4}\|Z(t)\|_{\Delta}^{2\mu} + \frac{\gamma\tau}{8\mu\rho_2M^{(2\mu-\tau)/\tau}}\lambda_2^{2\mu/\tau}, \quad (38)$$

where: $\rho_2 =: \left(\omega_2 + \frac{2\mu-\tau}{2\mu}\right)$.

Therefore, it follows from (33) and (38) that:

$$\begin{aligned} \dot{U}(Z(t)) &\leq -\left(\frac{\gamma M}{4}\|Z(t)\|_{\Delta}^{2\mu} + \frac{\gamma\tau}{8\mu\rho_2M^{(2\mu-\tau)/\tau}}\lambda_2^{2\mu/\tau}\right) + \frac{\gamma\tau}{8\mu\rho_2M^{(2\mu-\tau)/\tau}}\lambda_2^{2\mu/\tau} + a_2G_2(M) \\ &\leq -\frac{\gamma}{4\rho_2}U(Z(t)) + \bar{G}_2(M), \end{aligned} \quad (39)$$

where: $\bar{G}_2(M) = \frac{\gamma\tau}{8\mu\rho_2M^{(2\mu-\tau)/\tau}}\lambda_2^{2\mu/\tau} + a_2G_2(M)$.

In the rest of the proof, we are shown similarly as in [7,29] that the state $Z(t)$ of closed-loop system (18), (22), and (23) is well-defined on $[0, +\infty)$ and is globally bounded. Since $\bar{G}_2(M)$ is positive and strictly monotonically decreasing to zero as $M \rightarrow \infty$, it is easily seen that, for any given $\varepsilon > 0$, one can choose a sufficiently large $M \in \Omega$ so as to satisfy:

$$\omega_1^{-\frac{1}{2\mu}}\left(\frac{4\rho_2\bar{G}_2(M)}{\gamma}\right)^{\frac{1}{2\mu}} < \varepsilon \quad (40)$$

Next, introduce a subset by:

$$\Xi = \left\{ Z \in \mathbb{R}^{2n-1} \mid U(Z) \geq \frac{8\rho_2 \bar{G}_2(M)}{\gamma} \right\} \subset \mathbb{R}^{2n-1} \quad (41)$$

and let $Z(t)$ be the trajectory of (24) with an initial state $Z(0)$. Suppose $Z(t) \in \Xi$ for some $t \in [0, \infty)$. Then, using (38), it can be deduced that:

$$\dot{U}(Z(t)) \leq -\frac{\gamma}{4\rho_2} U(Z(t)) + \bar{G}_2(M) \leq -\bar{G}_2(M) < 0 \quad (42)$$

This means that, if $Z(t) \in \Xi$, $U(Z(t))$ will decrease strictly with respect to t . Therefore, in a finite time T , $Z(t)$ must enter $\mathbb{R}^{2n-1} - \Xi$ and stay there forever. Hence, one can obtain the following relations:

$$\begin{aligned} U(Z(t)) - U(Z(0)) &= \int_0^t \dot{U}(Z(t)) dt < 0, \quad t \in [0, T) \\ U(Z(t)) &< \left(\frac{8\rho_2 \bar{G}_2(M)}{\gamma} \right)^{\frac{2\mu-\tau}{2\mu}}, \quad t \in [T, \infty) \end{aligned} \quad (43)$$

which, together with (37), lead to:

$$\begin{aligned} |Z_i(t)| &\leq \|Z(t)\|_{\Delta}^{r_i} \leq \left(\frac{1}{\omega_1} U(Z(t)) \right)^{\frac{r_i}{2\mu}} \\ &\leq \omega_1^{-\frac{r_i}{2\mu}} U(Z(0))^{\frac{r_i}{2\mu}}, \quad t \in [0, T) \\ |Z_i(t)| &\leq \|Z(t)\|_{\Delta}^{r_i} \leq \left(\frac{1}{\omega_1} U(Z(t)) \right)^{\frac{r_i}{2\mu}} \\ &\leq \omega_1^{-\frac{r_i}{2\mu}} \left(\frac{8\rho_2 \bar{G}_2(M)}{\gamma} \right)^{\frac{r_i}{2\mu}}, \quad t \in [T, +\infty) \end{aligned} \quad (44)$$

For $i = 1, \dots, 2n - 1$. This implies that the trajectory $Z(t)$ of system (24) is well defined and globally bounded on $[0, +\infty)$.

Next, we prove that:

$$|y(t)| = |x_1(t) - y_r(t)| < \varepsilon, \quad \forall t \geq T > 0 \quad (45)$$

This can be easily seen from (35), (40), and (43) as follows:

$$\begin{aligned} |y(t)| &= |x_1(t) - y_r(t)| = |z_1(t)| \leq \|Z(t)\|_{\Delta} \\ &\leq \left(\frac{1}{\omega_1} U(Z(t)) \right)^{\frac{1}{2\mu}} \leq \omega_1^{-\frac{1}{2\mu}} \left(\frac{8\rho_2 \bar{G}_2(M)}{\gamma} \right)^{\frac{1}{2\mu}} < \varepsilon \end{aligned} \quad (46)$$

Finally, since the choice of $M \in \Omega$ depends on $\varepsilon > 0$, the finite time $T > 0$ depends on $\varepsilon > 0$. Further, it is obvious that $T > 0$ is dependent on each trajectory of (24), or equivalently on each initial state $Z(0)$ of (24). Therefore, the finite time $T > 0$ satisfying (46) is dependent on both $\varepsilon > 0$ and $Z(0)$, i.e., $T := T(\varepsilon, x(0), \zeta(0))$. \square

The process of control design shows that the lower triangular growth condition as required by Assumption 1 is not necessary for achieving the global practical output tracking of the system (1). In fact, we can extend Theorem 1 under the following assumption.

Assumption 3. For $i = 1, 2, \dots, n$, there are constants $C_1 > 0$, $C_2 > 0$, $M > 1$, $0 < \nu_i \leq 1$, and $\tau \geq 0$ such that:

$$\left| \frac{\varphi_i(\cdot)}{M^{\kappa_i}} \right| \leq C_1 M^{1-\nu_i} \sum_{j=1}^n \left(\left| \frac{x_j(t)}{M^{\kappa_j}} \right|^{(r_i+\tau)/r_j} + \left| \frac{x_j(t-d_j(t))}{M^{\kappa_j}} \right|^{(r_i+\tau)/r_j} \right) + \frac{C_2}{M^{\kappa_i}}, \quad (47)$$

where $\kappa_1 = 0$, $r_1 = 1$, $\kappa_{i+1} = (\kappa_i + 1)/p_i$, and $r_{i+1}p_i = r_i + \tau > 0$, $i = 1, \dots, n$.

It can be easily concluded that Assumption 1 is a special case of Assumption 3. The following theorem is a more general result on the global practical tracking of non-triangular systems.

Theorem 2. Under Assumptions 2 and 3, the problem of global practical tracking via output feedback controller of the form (22), (23) can be solved for system (1).

Proof . The proof is very similar to that of Theorem 1 and hence is omitted here. \square

5. Example and Simulation

The above method is used for the following numerical example considering the inherently nonlinear time delay system:

$$\begin{aligned} \dot{x}_1(t) &= x_2^{5/3}(t) + 0.25x_1^2(t) \sin(x_2(t)) \\ \dot{x}_2(t) &= u(t) + 0.125x_2^{5/3}(t - 0.2) \\ y(t) &= x_1(t) - y_r(t) \end{aligned} \quad (48)$$

For $p_1 = 5/3$, $\tau = 5/3$, $r_1 = 1$, $r_2 = 1$ and $\mu = 5/3$, it is not difficult to prove that system (48) satisfies the conditions of Assumption 1. Therefore, following the design procedure above, the output controller can be constructed as:

$$\begin{aligned} \dot{\eta}_2 &= -M^{3/5}(\eta_2 + L_1(x_1 - y_r)) \\ u &= -M^{8/5}\beta_2 \left(\beta_1(x_1 - y_r)^{5/3} + (\eta_2 + L_1(x_1 - y_r))^{5/3} \right) \end{aligned} \quad (49)$$

choosing $L_1 = 0.6$, $\beta_1 = 1.1$, $\beta_2 = 2.1$ and $M = 8$. In this simulation, the reference signal is chosen as $y_r(t) = \sin(t)$, and the initial condition is $x_1(0) = -2$, $x_2(0) = 0.1$ and $\eta_2(0) = 0$. From the following Figures 1–4, the effectiveness of the design procedure is verified.

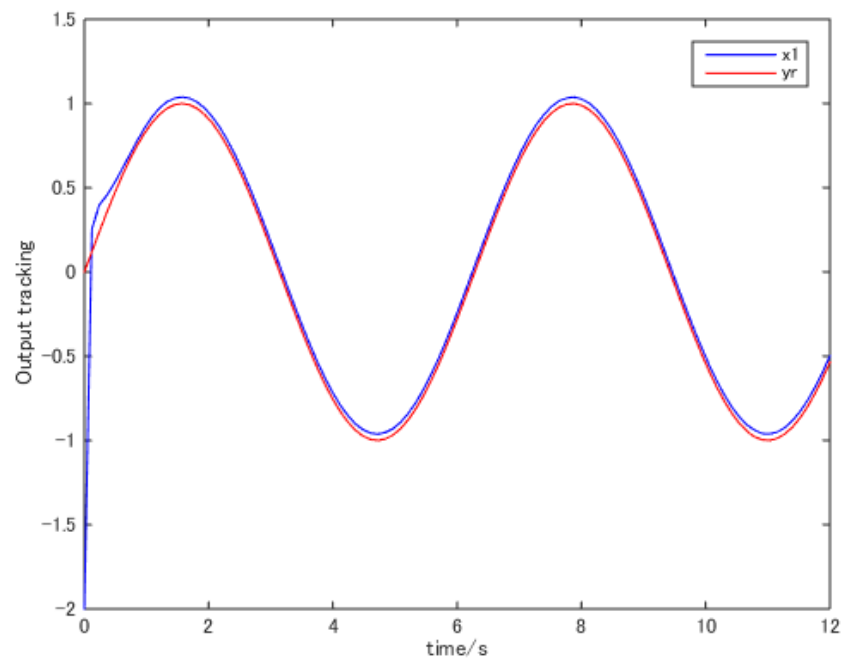


Figure 1. The trajectories of $x_1(t)$ and $y_r(t)$.

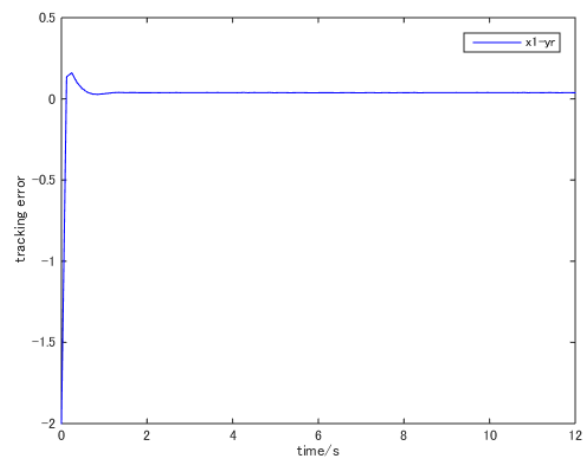


Figure 2. The trajectory of $x_1(t) - y_r(t)$.

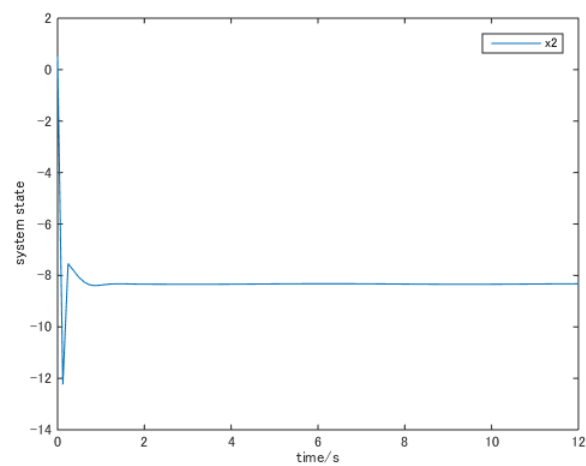


Figure 3. The trajectory of state $x_2(t)$.

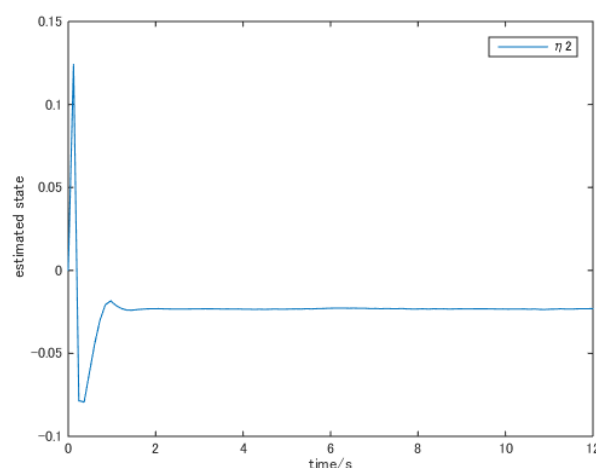


Figure 4. The trajectory of state $\eta_2(t)$.

6. Conclusions

In this work, we addressed the practical output feedback tracking problem for a class of high-order nonlinear time delay systems which cannot be handled by existing approaches. The proposed output controller independent of time delay can make the tracking error arbitrarily capable of being adjusted to be sufficiently small and render all the trajectory of the closed-loop system as are bounded. Our future study is to extend the proposed method for more inherently nonlinear time-varying delay systems.

Author Contributions: Conceptualization, K.A. and O.J.M.; methodology, K.A.; software, O.J.M.; validation, G.A.A., and A.A.; formal analysis, K.A.; investigation, K.A., and O.J.M.; resources, G.A.A.; data curation, A.A.; writing—original draft preparation, K.A.; writing—review and editing, O.J.M., G.A.A. and A.A.; visualization, G.A.A. and A.A. All authors have read and agreed to the published version of the manuscript.

Funding: This research has been funded by the Science Committee of the Ministry of Education and Science of the Republic Kazakhstan (Grant No. AP08855743).

Institutional Review Board Statement: Not applicable.

Informed Consent Statement: Not applicable.

Data Availability Statement: Not applicable.

Acknowledgments: The authors are very thankful to the editor and referees for their valuable comments and suggestions for improving the paper.

Conflicts of Interest: The authors declare no conflict of interest.

References

1. Čelikovský, S.; Huang, J. Continuous feedback practical output regulation for a class of non-linear systems having non-stabilizable linearization. In Proceedings of the 38th IEEE Conference on Decision and Control, Phoenix, AZ, USA, 7–10 December 1999; pp. 4796–4801.
2. Qian, C.; Lin, W. Practical output tracking of nonlinear systems with uncontrollable unstable linearization. *IEEE Trans. Autom. Control*. **2002**, *47*, 21–36. [[CrossRef](#)]
3. Lin, W.; Pongvuthithum, R. Adaptive output tracking of inherently nonlinear systems with nonlinear parameterization. *IEEE Trans. Autom. Control*. **2003**, *48*, 1737–1749. [[CrossRef](#)]
4. Gong, Q.; Qian, C. Global Practical Output Regulation of a Class of Nonlinear Systems by Output Feedback. *Automatica* **2007**, *43*, 184–189. [[CrossRef](#)]
5. Sun, Z.-Y.; Liu, Y.-G. Adaptive Practical Output Tracking Control for High-order Nonlinear Uncertain Systems. *Acta Autom. Sin.* **2008**, *34*, 984–989. [[CrossRef](#)]
6. Alimhan, K.; Inaba, H. Practical output tracking by smooth output compensator for uncertain nonlinear systems with unstabilizable and undetectable linearization. *Int. J. Model. Identif. Control* **2008**, *5*, 1–13. [[CrossRef](#)]
7. Alimhan, K.; Inaba, H. Robust practical output tracking by output compensator for a class of uncertain inherently non-linear systems. *Int. J. Model. Identif. Control*. **2008**, *4*, 304. [[CrossRef](#)]

8. Bi, W.P.; Zhang, J.F. Global practical tracking control for high-order nonlinear uncertain systems. In Proceedings of the Chinese Control and Decision Conference, Xuzhou, China, 26–28 May 2010; pp. 1619–1622.
9. Yan, X.; Liu, Y. Global Practical Tracking for High-Order Uncertain Nonlinear Systems with Unknown Control Directions. *SIAM J. Control. Optim.* **2010**, *48*, 4453–4473. [[CrossRef](#)]
10. Yan, X.; Liu, Y. Global practical tracking by output-feedback for nonlinear systems with unknown growth rate. *Sci. China Inf. Sci.* **2011**, *54*, 2079–2090. [[CrossRef](#)]
11. Zhai, J.; Fei, S. Global practical tracking control for a class of uncertain non-linear systems. *IET Control. Theory Appl.* **2011**, *5*, 1343–1351. [[CrossRef](#)]
12. Alimhan, K.; Otsuka, N. *A Note on Practically Output Tracking Control of Nonlinear Systems That May not Be Linearizable at the Origin. Communications in Computer and Information Science*; Springer: Berlin/Heidelberg, Germany, 2011; Volume 256 CCIS, pp. 17–25.
13. Yan, X.; Liu, Y. The further result on global practical tracking for high-order uncertain nonlinear systems. *J. Syst. Sci. Complex.* **2012**, *25*, 227–237. [[CrossRef](#)]
14. Alimhan, K.; Otsuka, N.; Adamov, A.A.; Kalimoldayev, M.N. Global practical output tracking of inherently non-linear systems using continuously differentiable controllers. *Math. Probl. Eng.* **2015**, *2015*, 932097. [[CrossRef](#)]
15. Alimhan, K.; Otsuka, N.; Kalimoldayev, M.N.; Adamov, A.A. Output Tracking Problem of Uncertain Nonlinear Systems with High-Order Nonlinearities. In Proceedings of the 2015 8th International Conference on Control and Automation, Jeju, Korea, 25–28 November 2015; pp. 1–4.
16. Guo, L.-C. Practical tracking control for stochastic nonlinear systems with polynomial function growth conditions. *Automatika* **2019**, *60*, 443–450. [[CrossRef](#)]
17. Alimhan, K.; Otsuka, N.; Kalimoldayev, M.N.; Tasbolatuly, N. Output Tracking by State Feedback for High-Order Nonlinear Systems with Time-Delay. *J. Theor. Appl. Inf. Technol.* **2019**, *97*, 942–956.
18. Alimhan, K.; Mamyrbayev, O.; Erdenova, A.; Akmetkalyeva, A. Global output tracking by state feedback for high-order nonlinear systems with time-varying delays. *Cogent Eng.* **2020**, *7*, 1711676. [[CrossRef](#)]
19. Sun, Z.; Liu, Y.; Xie, X. Global stabilization for a class of high-order time-delay nonlinear systems. *Int. J. Innov. Comput. Inf. Control* **2011**, *7*, 7119–7130.
20. Sun, Z.; Xie, X.; Liu, Z. Global stabilization of high-order nonlinear systems with multiple time delays. *Int. J. Control* **2013**, *86*, 768–778. [[CrossRef](#)]
21. Sun, Z.; Zhang, X.; Xie, X. Continuous global stabilization of high-order time-delay nonlinear systems. *Int. J. Control* **2013**, *86*, 994–1007. [[CrossRef](#)]
22. Chai, L. Global Output Control for a Class of Inherently Higher-Order Nonlinear Time-Delay Systems Based on Homogeneous Domination Approach. *Discret. Dyn. Nat. Soc.* **2013**, *2013*, 1–6. [[CrossRef](#)]
23. Zhang, N.; Zhang, E.; Gao, F. Global Stabilization of High-Order Time-Delay Nonlinear Systems under a Weaker Condition. *Abstr. Appl. Anal.* **2014**, *2014*, 1–8. [[CrossRef](#)]
24. Gao, F.; Wu, Y. Further results on global state feedback stabilization of high-order nonlinear systems with time-varying delays. *ISA Trans.* **2015**, *55*, 41–48. [[CrossRef](#)] [[PubMed](#)]
25. Gao, F.; Wu, Y. Global stabilisation for a class of more general high-order time-delay nonlinear systems by output feedback. *Int. J. Control.* **2015**, *88*, 1–14. [[CrossRef](#)]
26. Zhang, X.; Lin, W.; Lin, Y. Nonsmooth Feedback Control of Time-Delay Nonlinear Systems: A Dynamic Gain Based Approach. *IEEE Trans. Autom. Control.* **2016**, *62*, 438–444. [[CrossRef](#)]
27. Yan, X.; Song, X. Global Practical Tracking by Output Feedback for Nonlinear Systems with Unknown Growth Rate and Time Delay. *Sci. World J.* **2014**, *2014*, 1–7. [[CrossRef](#)] [[PubMed](#)]
28. Jia, X.; Xu, S.; Chen, J.; Li, Z.; Zou, Y. Global output feedback practical tracking for time-delay systems with uncertain polynomial growth rate. *J. Frankl. Inst.* **2015**, *352*, 5551–5568. [[CrossRef](#)]
29. Jia, X.; Xu, S. Global practical tracking by output feedback for nonlinear time-delay systems with uncertain polynomial growth rate. In Proceedings of the 2015 34th Chinese Control Conference (CCC), Hangzhou, China, 28–30 July 2015; pp. 607–611.
30. Jia, X.; Xu, S.; Ma, Q.; Qi, Z.; Zou, Y. Global practical tracking by output feedback for a class of non-linear time-delay systems. *IMA J. Math. Control. Inf.* **2016**, *33*, 1067–1080. [[CrossRef](#)]
31. Rosier, L. Homogeneous Lyapunov function for homogeneous continuous vector field. *Syst. Control. Lett.* **1992**, *19*, 467–473. [[CrossRef](#)]
32. Polendo, J.; Qian, C. A generalized homogeneous domination approach for global stabilization of inherently nonlinear systems via output feedback. *Int. J. Robust Nonlinear Control.* **2007**, *17*, 605–629. [[CrossRef](#)]
33. Polendo, J.; Qian, C. A universal method for robust stabilization of nonlinear systems: Unification and extension of smooth and non-smooth approaches. In Proceedings of the 2006 American Control Conference, Minneapolis, MN, USA, 14–16 June 2006.
34. Zhai, J.-Y. Finite-Time Output Feedback Stabilization for Stochastic High-Order Nonlinear Systems. *Circuits Syst. Signal Process.* **2014**, *33*, 3809–3837. [[CrossRef](#)]
35. Zhai, J.-Y.; Du, H.-B. Global output feedback stabilisation for a class of upper triangular stochastic nonlinear systems. *Int. J. Control.* **2014**, *87*, 1–12. [[CrossRef](#)]
36. Zhai, J.-Y.; Song, Z.; Karimi, H.R. Global finite-time control for a class of switched nonlinear systems with different powers via output feedback. *Int. J. Syst. Sci.* **2018**, *49*, 2776–2783. [[CrossRef](#)]